

LABORATORY MEASUREMENT OF IMPACT SOUND INSULATION OF A FLOORING SYSTEM (According to ISO 10140-3)

AUCKLAND UNISERVICES LIMITED a wholly owned company of THE UNIVERSITY OF AUCKLAND

Report prepared for:

Resene Construction Systems Ltd PO Box 58317 Botany Manakau 2163 Auckland

Date: 28th October 2016

Report prepared by:

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LABORATORY
MEASUREMENT OF
IMPACT SOUND
INSULATION OF A TONGUE
AND GROOVE FLOORING
SYSTEM

Prepared For: Resene Construction Systems Ltd

PO Box 58317 Botany Manakau 2163 New Zealand

Prepared by: Acoustics Testing Service

Department of Mechanical Engineering

University of Auckland

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Normalized Impact sound pressure levels according to ISO 10140-3 Laboratory measurements of impact sound insulation of floors

Description and identification of the test specimen and test arrangement:

Date of test: 8-Mar-16 Client: Rockcote Resene Ltd.

Test Floor Frame: 190mm x 45mm timber joists set at 450mm centres

Test Floor Linings: Source chamber side: Rockcote Resene Integra tongue and groove flooring panels

Receiving chamber side: 2 layers of 13mm GIB Noiseline on 28mm furring channel in ST001 clipsscrew-fixed to the under side of the

timber joists

Cavity Absorption: 1 layer of *Pink Batts* Mid Floor Silencer batts
Test Floor Lining Joint Filler: *GIB Soundseal*

Test Floor Perimeter Sealant: GIB Soundseal

Source chamber: Chamber B, Receiving chamber: Chamber A. Test specimen installed by client. Curing time:

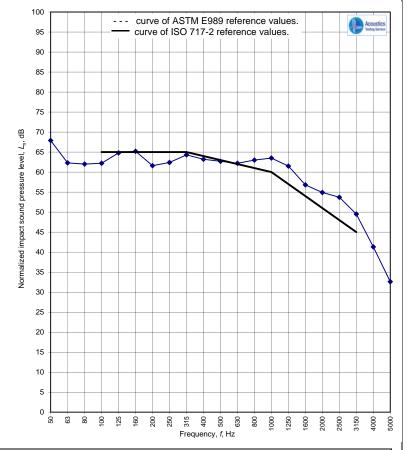
Computer files: T1608-3 Floor with 2x13mm NL.CMG; T1608-3 Floor with 2x13mm NL.CMG

Area S of test specimen:	10.24 m ²
Air temp in the test rooms:	21 °C
Air humidity in test rooms:	60 %
Source room volume:	202 m ³
Receiving room volume:	153 m ³

Frequency f One-third octave Hz dB 50 67.9 63 62.3 80 62.0 100 62.2 125 64.8 160 65.2 200 61.6 250 62.4 315 64.3 400 63.2 500 62.7 630 62.2 800 63.0 1000 63.5 1250 61.5 1600 56.8 2000 54.9 2500 53.7 3150 49.5 4000 41.3	Receiving room volume:		153
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200 61.6 250 62.4 315 64.3 400 63.2 500 62.7 630 62.2 800 63.0 1000 63.5 1250 61.5 1600 56.8 2000 54.9 2500 53.7 3150 49.5 4000 41.3	125	64.8	
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315 64.3 400 63.2 500 62.7 630 62.2 800 63.0 1000 63.5 1250 61.5 1600 56.8 2000 54.9 2500 53.7 3150 49.5 4000 41.3	200	61.6	
400 63.2 500 62.7 630 62.2 800 63.0 1000 63.5 1250 61.5 1600 56.8 2000 54.9 2500 53.7 3150 49.5 4000 41.3	250	62.4	
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1000 63.5 1250 61.5 1600 56.8 2000 54.9 2500 53.7 3150 49.5 4000 41.3	630	62.2	
1250 61.5 1600 56.8 2000 54.9 2500 53.7 3150 49.5 4000 41.3	800	63.0	
1600 56.8 2000 54.9 2500 53.7 3150 49.5 4000 41.3	1000	63.5	
2000 54.9 2500 53.7 3150 49.5 4000 41.3	1250	61.5	
2500 53.7 3150 49.5 4000 41.3	1600	56.8	
3150 49.5 4000 41.3	2000	54.9	
4000 41.3	2500	53.7	
1	3150	49.5	
	4000	41.3	
5000 32.6	5000	32.6	



- 2. Bold values are used to
- IIC and Ln,w. 3. Words in Blue Italic in the
- description are manufacturers brand names.
- 4. < indicates that the true value is lower.



Rating according to ISO 717-2:

$$L_{n,w}$$
 (C_1) = 63 (-4) dB

 $C_{1,50-2500} = -2 \text{ dB}$

Rating according to ASTM E989:

Impact Insulation Class = 47 dB

Evaluation based on laboratory measurement results obtained by an engineering method.

No. of test report: T1608-3

Name of test institute: University of Auckland Acoustics Testing Service.

Date: Friday, 28 October 2016

Signature:



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Figure 1: Floorboard sitting on frame



Figure 2: Floor frame installed in floor cavity



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Figure 3: One of the tapping machine positions on the floor



Figure 4: Tapping machine placed on floorboards



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INSTRUMENTATION	EQUIPMENT	TYPE / SERIAL No.	
	SOURCE ROOM		
	1/2" Microphone	4190 / 2143842	
	Preamplifier	2619 / 945932	
	Rotating Boom	3923 / 936486	
	RECEIVING ROOM		
	1/2" Microphone	4190 / 2143842	
	Preamplifier	2619 / 945932	
	Rotating Boom	3923 / 936486	
	Calibration of the above equipment	was conducted by Electroacoustic	
	Calibration Services (ECS), an IANZ registered laboratory.		
	BRÜEL & KJÆR		
	Pistonphone	4220 / 1048366	
	Analyzer	2133 / 1529583	
	Tapping Machine	3204 / 250841	



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SUMMARY OF THE MEASUREMENT OF SOUND IMPACT INSULATION IN FLOORS.

INSTALLATION OF TEST SAMPLE

The floor/ceiling system under test is installed in the opening between the two large reverberation chambers – chambers B and A. These chambers are vibration isolated from each other which results in a structural discontinuity at the middle of the test opening. This gap is covered over by a wooden collar, which seals the gap and provides for ease of fixing of samples The sample is constructed by the client following the techniques normally used in practice for that type of floor/ceiling system, and is sealed into the test opening with perimeter seals of acoustic sealant.

METHOD

The normalized impact sound pressure levels are obtained in accordance with the recommendations of ISO standard 140-6:1998(E) "Laboratory measurements of impact sound insulation of floors."

The BK3204 tapping machine is placed sequentially in four different positions on the floor. The impact sound pressure level is measured in the room below the floor, using a rotating microphone, in third octave frequency bands. The impact sound pressure levels are normalized against the room absorption. The room absorption is calculated from the reverberation time and room volume. The reverberation time is measured from the decay of a steady state sound field.

Corrections are applied, where necessary, for airborne sound transmission and background noise. The airborne sound transmission is determined using a loudspeaker and the microphone.

RESULTS

The third octave band normalized impact sound pressure levels $L_{\rm n}$ are presented in both table and graph formats. Sometimes a highly reflective test sample means that the lower frequency normalized impact sound pressure levels cannot be reliably measured; this is indicated by #N/A in the table of results. Additionally, sometimes the airborne transmission of sound through the floor or loud background noise affects the measurements resulting in only an upper threshold being found; this is indicated by a < sign preceding the tabulated results.

Single figure ratings are also presented. The weighted normalized impact sound pressure level $L_{n,w}$, determined according to ISO 717-2, is presented along with a spectrum adaptation term C_1 . $L_{n,w}$ is determined by fitting a reference curve to the third octave band normalized impact sound pressure levels L_n from 100Hz to 3150Hz, and gives a single figure determination of the sound levels which are transmitted through the floor from impacts (higher is worse). The spectrum adaptation term C_1 is used to suggest the presence of high level peaks in the results over the frequency range 100Hz to 2500Hz, and may be added to $L_{n,w}$. For massive floors with effective coverings C_1 will be about zero, for light timber floors C_1 will be slightly positive, and for concrete floors with less effective covering C_1 will range from -15 dB to 0dB. Another spectrum adaptation term $C_{1,50-2500}$, which covers the frequency range from 50Hz to 2500Hz, may also be presented if the low frequency levels are available.

The impact insulation class (IIC) determined according ASTM E989 is also presented. This is determined by fitting a reference curve to the third octave band normalized impact sound pressure levels $L_{\rm n}$ from 100Hz to 3150Hz, but in a slightly different way to ISO 717-2. The impact insulation class measures the insulating abilities of the floor so that higher is better (contrary to $L_{\rm n,w}$).



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There are three large interconnected reverberation chambers at the Acoustics Research Centre, two at ground level (Chambers C and A) and the third (Chamber B) below A.

All three reverberation chambers may be described as hexagonal prisms; each has 6 vertical sided walls, perpendicular to the floor. The roofs of chamber A and C are plane, but inclined at 12 degrees from horizontal. Chamber B has a plane, horizontal roof which is the floor of chamber A above it. The floor of chamber B is also horizontal, but has two angled sections at its North West and south east ends. The centre section is horizontal because a floor jack is installed there. The floor jack may be raised hydraulically to the ceiling of chamber B, the centre of which consists of a floor plug between the two chambers. This plug may be disconnected from chamber A and lowered down into chamber B, leaving a 3.2m x 3.2 m opening between the two chambers. This allows for the measurement of airborne and impact insulation of floor and roof elements.

The wall of chamber C adjacent to chamber A is left open, and the corresponding wall of chamber A consists of a pair of iron doors that are clamped against the chamber. The clamps may be removed and the iron doors pulled back, leaving the entire wall area (4.6m wide x 2.74m high) between the chambers open. This allows for the measurement of airborne sound insulation of wall elements.

Chamber A has a rotating vane diffuser in a central position with an area (both sides) of about 53 m2. It has the shape of two cones with their bases joined, with the two opposite quadrants of one cone open and the complementary quadrants in the other cone open. Chamber C has a similar rotating vane diffuser but it is smaller, having a total area of about 27 m2.

In addition, up to ten static diffusers may be employed if needed. These are constructed of two laminated layers of dense Formica, of dimensions 1m x 1m. The Formica elements are riveted to a frame constructed of aluminium T section. Four aluminium arms may be bolted onto the frame to allow the diffusers to be mounted as desired. Currently four of these are used in chamber C, and three are used in chamber B.

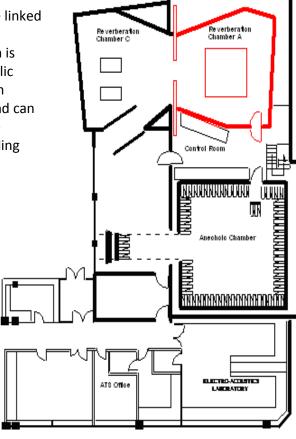
The volumes and surface areas of the reverberation chambers are as follows:

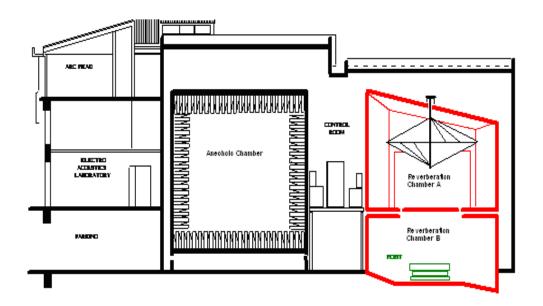
	VOLUME (m³)	SURFACE AREA (m²)
Chamber A	202 ± 3	203.6 ± 0.9
Chamber B	153 ± 2	173 ± 1
Chamber C	209 ± 4	214 ± 0.9



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The three Reverberation Chambers are linked by heavy steel doors and a removable Standard Industrial Floor Section which is removed and repositioned by a hydraulic hoist. The three chambers are vibration isolated from one another so that sound can only pass from one to the other via the intervening Test Wall or Test Floor/Ceiling Section







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